

AESB 2320 Part 2 Exam 19 April 2017

1. How does this differ from section 9.2 of BSL1?

- different B.C. at $r=R$ (Newton's law of cooling)
- non-uniform generation function $S_e(r)$.

The B.C. does not affect the shell balance. Newton's law of cooling does not interact with the control volume between r and $(r+\Delta r)$. It doesn't enter the derivation until Eq. 9.2-12. The non-uniform S_e , however, alters the integration of Eq. 9.2-6 to 9.2-7. Eq. 9.2-7 assumes S_e is a constant. Therefore the last equation that applies is Eq. 9.2-6.

(This same issue came up in the Part 1 exam (15 March), problem 1. There, the nonuniform viscosity μ meant that one could not integrate for q_{rz} assuming μ is constant.)

2. a) Newton's law of cooling: specifies $q_r = h(T - T_a)$

b) A macroscopic energy balance on the cylinder:

rate of heat lost to surroundings: $(2\pi RL)h(T - T_a)$

a accumulation: $(\pi R^2 L)\rho c_p \frac{dT}{dt}$

no generation, no convection

$$-(2\pi RL + 2\pi R^2)h(T - T_a) = \pi R^2 L \rho c_p \frac{dT}{dt}$$

$$\frac{d(T - T_a)}{dt} = - \frac{2\pi RL h}{\pi R^2 L \rho c_p}$$

$$= - \frac{2h}{R \rho c_p}$$

$$\frac{d(T - T_a)}{T - T_a} = - \frac{2h}{R \rho c_p} t$$

$$\ln(T - T_a) = - \frac{2h}{R \rho c_p} t + C_1$$

at $t=0$, $\ln(T - T_a) = \ln(200 - 20)$

$$\frac{T - 20}{200 - 20} = \exp\left(- \frac{2h}{R \rho c_p} t\right) = \exp\left(- \frac{2(50)}{(0.025)(1100)(350)} t\right)$$

$$= \exp(-2.79 \cdot 10^{-3} t)$$

c) There was some confusion among students on the meaning of "gradient," which means derivative with respect to position (dt/dr), not time (dt/dt). As it happens, the maximum in both (dt/dr) and (dt/dt) occurs at $t=0$.

From Fourier's law in the solid,

$$q_r = -k(dt/dr)$$

Since the heat flux at the surface is given by Newton's law of cooling, then at the surface

$$-k \frac{dT}{dr} = h(T - T_a)$$

The maximum in $(T - T_a)$ occurs at $t=0$; it decreases with time.

$$\left. \frac{dT}{dr} \right|_{r=R, t=0} = -\frac{q_r}{k} = -\frac{h(T - T_a)}{k} = -\frac{h(180)}{k} = -\frac{50(180)}{35} = 257 \frac{^\circ K}{m}$$

3. Convective heat transfer is in series with internal convection. For processes in series, the slow step controls; therefore we want internal convection to be as fast as possible compared to convective heat transfer to the surface.

Internal conduction depends on $\frac{\alpha t}{R^2}$, with $\alpha = \frac{k}{\rho c_p}$.

For convective heat transfer, leading to a macroscopic energy balance like that in problem 2(b), temperature scales with $\frac{ht}{\rho c_p}$ (see problem 2). Both processes slow down as ρc_p increases, but a larger k makes internal conduction go faster. Therefore the best metal has the larger k . Metal A has 10x larger k ; it is the better choice, even though (ρc_p) is larger.

[When I first wrote this problem, I thought the only thing that matters is α . I also accepted answers specifying metal A, because α is about 6x larger, though the complete answer is more complicated.]

4. Because of the perfectly insulated surface, this problem is equivalent to a cube, 0.2 m on a side, where we calculate T at center.

$$\alpha = \frac{k}{\rho c_p} = \frac{23}{7820 \cdot 461} = 6.38 \times 10^{-6}$$

At 5 mm, $\frac{\alpha t}{b^2} = \frac{6.38 \cdot 10^{-6} (500)}{(0.1)^2} = 0.19$

From chart for slab, $\frac{T_1 - T}{T_1 - T_0} \approx 0.77$ at $\frac{x}{b} = 0$

for cube, " $= (0.77)^3 = 0.46$

$$\frac{100 - T}{100 - 0} = 0.46 ; T = 54^\circ\text{C}$$

at 8 mm, $\frac{\alpha t}{b^2} = \frac{6.38 \cdot 10^{-6} (450)}{(0.1)^2} = 0.306$

from chart for slab, $\frac{T_1 - T}{T_1 - T_0} = 0.6$ at $x/b = 0$

for cube, " $= (0.6)^3 = 0.29$

$$\frac{T_1 - T}{T_1 - T_0} = 0.29 = \frac{100 - T}{100 - 0} \Rightarrow T = 0.71^\circ\text{C}$$

5. For this problem, we need $\frac{T - T_0}{T_1 - T_0}$. We already solved for $\frac{T_1 - T}{T_1 - T_0}$ in problem 4.

At 8 mm $\frac{T - T_0}{T_1 - T_0} = \frac{71 - 0}{100 - 0} = 0.71$

5 mm " $\frac{54 - 0}{100 - 0} = 0.54$

Dimensionless T is $\frac{T - 0}{100 - 0}$. Second change is opposite to first

$$\frac{T - T_0}{T_1 - T_0} = \left(\frac{T - T_0}{T_1 - T_0} \right)_{8 \text{ mm}} - \left(\frac{T - T_0}{T_1 - T_0} \right)_{5 \text{ mm}} = 0.71 - 0.54 = 0.17$$

$$\frac{T - 0}{100 - 0} = 0.17 ; T = 17^\circ\text{C}$$